# Break-Away Torque Calculation for 2 Gear Rotor Shafts

Below is an example calculation method for the "initial torque" which must be used by the driving machine to achieve dynamic rotation from a static condition. This is based on the gear rotor set coupled to the rotor of the driven machine. Both the "direction of rotation" and the "break-away torque of the driven rotor (compressor/generator)" must be known since the final friction strengths are dependent on the calculation for the gearing.

# Calculation for 2 rotor shafts



### <u>Shaft 2 – Driven Rotor</u>

Rotational force required for taking into account the driven machines break-away torque

$$F_{U_2} = 1000 \cdot \frac{M_{L2}}{R_2}$$

Net breaking force for driven rotor bearings derived from  $F_{U_2}$  and  $G_2$ 

 $L_2 = F_{U_2} \pm G_{2_{[2]}}$ 

 $G_2$  is negative if force direction on driven rotor mesh is  $up \uparrow (up mesh)$  $G_2$  is positive if force direction on driven rotor mesh is down  $\downarrow$  (down mesh)

Net Rotational Force to overcome bearing friction on driven rotor

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$$F_2 = \frac{L_2 \cdot \mu}{\frac{R_2}{r_2} \mp \mu}$$

 $\mu$  is positive if force direction on driven rotor mesh is up  $\uparrow$  (up mesh)  $\mu$  is negative if force direction on driven rotor mesh is down  $\downarrow$  (down mesh)

Total driven rotor force

$$F_{U_{12}} = F_{U_2} + F_2_{[4]}$$

Shaft 1 – Driving Rotor

Force on driving rotor derived from  $F_u$  and  $G_1$ 

$$L_1 = F_{u_{12}} \pm G_{1_{5}}$$

 $G_1$  is **positive** if force direction on driving rotor mesh is down  $\downarrow$  (up mesh)  $G_1$  is **negative** if force direction on driving rotor mesh is up  $\uparrow$  (down mesh)

Total combined moment due to friction from both driving/driven Rotors

$$M_{R_{\rm i}} = \frac{L_{\rm i} \cdot \mu \cdot r_{\rm i}}{1000}$$
[6]

Total Break-Away Torque for this rotor set

$$M_{L_{zer}} = \frac{F_{U_{12}} \cdot R_1}{1000} + M_{R_1} (+ M_{L_1})$$
<sup>[7]</sup>

- including the coupled machine

The driver is like a shaft rope coupled to the drive. Unlike the driven break-away torque, the driver break-away torque  $M_{L1}$  does not have any influence on the gearing. This is added to the total break-away torque of the gearing at the drive flange.

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# EXAMPLE:

$$\begin{split} &M_{L_2} = 400 \text{ Nm} \text{ - assumed break-away torque of driven machine} \\ &G_2 = 5000 \text{ N} \text{ - wheel rotor weight} \\ &R_2 = 200 \text{ mm} \text{ - wheel pitch line radius} \\ &r_2 = 65 \text{ mm} \text{ - wheel journal radius} \\ &G_1 = 2000 \text{ N} \text{ - pinion rotor weight} \\ &R_1 = 140 \text{ mm} \text{ - pinion pitch line radius} \\ &r_1 = 45 \text{ mm} \text{ - pinion journal radius} \\ &\mu = 0.26 \text{ - friction factor} \end{split}$$



### Shaft 2: Shaft 1:

 $F_{U_2} = 1000 \cdot \frac{400}{200} = 2000 \, \Uparrow \, Nm \ L_1 = 2234 \, \Downarrow \, +2000 \, \Downarrow = 4234 \, \Downarrow \, N$ 

$$L_2 = 2000 \text{ ft} -5000 \text{ Jt} = 3000 \text{ Jt} N M_R = \frac{4234 \cdot 0.26 \cdot 45}{1000} = 49.5N$$

$$F_2 = \frac{3000 \cdot 0.26}{\frac{200}{65} + 0.26} = 234N$$
$$M_{1_{set}} = \frac{2234 \cdot 140}{1000} + 49.5 = \underline{362.3Nm}$$

$$F_{U_{12}} = 2000 + 234 = 2234 \text{ ft } N$$

note: add M<sub>L1</sub> to obtain the total drive train break away torque

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